DIRC for a Higher Luminosity B Factory

Thomas Hadig
Stanford Linear Accelerator Center, Stanford University, Stanford, CA 94309
for the BaBar-DIRC Collaboration[1]

Abstract

The DIRC, a novel type of Cherenkov ring imaging device, is the primary hadronic particle identification system for the BaBar detector at the asymmetric B-factory PEP-II at SLAC. It is based on total internal reflection and uses long, rectangular bars made from synthetic fused silica as Cherenkov radiators and light guides. BaBar began taking data with colliding beams in late spring 1999. This paper describes the challenges for the DIRC in a higher luminosity environment and shows solutions to these challenges.

1 Introduction

The study of CP-violation using hadronic final states of the $B\bar{B}$ meson system requires the ability to tag the flavor of one of the $B$ mesons via the cascade decay $b \rightarrow c \rightarrow s$, while fully reconstructing the final state of the other over a large region of solid angle and momentum. The momenta of the kaons used for flavor tagging extend up to about 2 GeV/c, with most of them below 1 GeV/c. On the other hand, pions from the rare two-body decays $B_0 \rightarrow \pi^+ \pi^- (K^+ \pi^-)$ must be well-separated from kaons. They have momenta between 1.7 GeV/c and 4.2 GeV/c with a strong momentum-polar angle correlation between the tracks (higher momenta occur at the more forward angles because of the c.m. system boost)[2]. The Particle Identification (PID) system in BaBar[3] is located inside the calorimeter volume. Therefore, it should be thin and uniform in terms of radiation lengths (to minimize degradation of the calorimeter energy resolution) and small in the radial dimension to reduce the volume, hence, the cost of the calorimeter.

The PID system being used in BaBar is a new kind of ring-imaging Cherenkov detector called the DIRC[4] (the acronym DIRC stands for Detection of Internally Reflected Cherenkov light). It is designed to be able to provide excellent $\pi/K$ separation for all tracks from $B$-meson decays from the pion Cherenkov threshold up to 4.2 GeV/c. PID below 700 MeV/c exploits also the $dE/dx$ measurements in the silicon vertex tracker and drift chamber.

2 DIRC Concept

The DIRC is based on the principle that the absolute values of angles are maintained upon reflection from a flat surface. Figure 1 shows a schematic of the DIRC geometry that illustrates the principles of light production, transport, and imaging. The radiator material of the DIRC is synthetic, fused silica in the form of long, thin bars with rectangular cross section. These bars serve both as radiators and as light pipes for the portion of the light trapped in the radiator by total internal reflection. Fused, synthetic silica (Spectrosil[5]) is chosen because of its resistance to ionizing radiation, its long attenuation length, large index of refraction, small chromatic dispersion within the wavelength acceptance of the DIRC, and because it allows an excellent surface polish on the bars[6].
In the following, the variable $\theta_C$ is used to designate the Cherenkov angle, $\phi_C$ denotes the azimuthal angle of a Cherenkov photon around the track direction, and $n$ represents the mean index of refraction of fused silica ($n = 1.473$) within the wavelength acceptance of the Dirc (300 nm to 600 nm). The Cherenkov angle is given by the familiar relation $\cos \theta_C = 1/(n\beta)$ with $\beta = v/c$, the velocity of the particle $v$ and the velocity of light $c$.

For particles with $\beta \approx 1$, some photons will always lie within the total internal reflection limit, and will be transported to either one or both ends of the bar, depending on the particle incident angle. To avoid instrumenting both ends of the bar with photon detectors, a mirror is placed at the forward end, perpendicular to the bar axis, to reflect incident photons to the backward, instrumented end (see Figure 1).

Once photons arrive at the instrumented end, most of them emerge into a water-filled expansion region, called the standoff box. A fused silica wedge at the exit of the bar reflects photons at large angles relative to the bar axis. It thereby reduces the size of the required detection surface and recovers those photons that would otherwise be lost due to internal reflection at the fused silica/water interface. The photons are detected by an array of densely packed photomultiplier tubes (PMTs)[7, 8], each surrounded by reflecting light catcher cones[9] to capture light which would otherwise miss the active area of the PMT. The PMTs are placed at a distance of about 1.2 m from the end of the bars. The expected Cherenkov light pattern at this surface is essentially a conic section, where the cone opening-angle is the Cherenkov production angle modified by refraction at the exit from the fused silica window.

The Dirc bars are arranged in a 12-sided polygonal barrel (see Figure 2). Because of the beam energy asymmetry (at the $\Upsilon(4S)$, Pep-II collides 9 GeV electrons on 3.1 GeV positrons), particles are produced preferentially forward in the laboratory. To minimize interference with other detector systems in the forward region, the Dirc photon detector is placed at the backward end. The bars are placed into 12 hermetically sealed containers, called bar boxes, made of aluminum-hexcel panels. Dry nitrogen gas flows through each box, and is monitored for humidity to ensure that the bar box to water interface remains sealed. Each bar box contains 12 bars, for a total of 144 bars. Within a bar box the 12 bars are optically isolated by a $\sim 150$ $\mu$m air gap between

Figure 1: Schematic of the Dirc fused silica radiator bar and imaging region.
neighboring bars, enforced by custom shims made from aluminum foil.

The bars are 17 mm thick, 35 mm wide, and 4.9 m long. Each bar is assembled from four 1.225 m pieces that are glued end-to-end; this length is the longest high-quality bar currently obtainable[6, 10]. The bars are supported at 600 mm intervals by small nylon buttons for optical isolation from the bar box. Each bar has a fused silica wedge glued to it at the readout end. The wedge, made of the same material as the bar, is 91 mm long with very nearly the same width (33 mm) as the bars and a trapezoidal profile (27 mm high at bar end, and 79 mm high at the light exit end). The bottom of the wedge (see Figure 1) has a slight (∼ 6 mrad) upward slope to minimize the displacement of the downward reflected image due to the finite bar thickness. The 12 wedges in a bar box are glued to a common 10 mm thick fused silica window which provides the interface and seal to the purified water in the standoff box.

The standoff box (see Figure 2) is made of stainless steel, consisting of a cone, cylinder, and 12 sectors of PMTs. It contains about 6000 l of purified water. Water is used to fill this region because it is inexpensive and has an average index of refraction ($n \approx 1.346$) reasonably close to that of fused silica, thus minimizing the total internal reflection at silica-water interface. Furthermore, its chromaticity index is a close match to that of fused silica, effectively eliminating dispersion at the silica-water interface. The iron gusset supports the standoff box. An iron shield, supplemented by a bucking coil, surrounds the standoff box to reduce the field in the PMT region to below 1 G[11].

The PMTs at the rear of the standoff box lie on an approximately toroidal surface. The distance from the end of the bar to the PMTs is ∼ 1.17 m. Each of the 12 PMT sectors contains 896 PMTs (ETL model 9125[7, 8]) with 29 mm diameter, in a closely packed array inside the water volume. A double o-ring water seal is made between the PMTs and the vessel wall. The PMTs are installed from the inside of the standoff box and connected via a feed-through to a base mounted outside. The hexagonal light catcher cone is mounted in front of the photocathode of each PMT which results in an effective active surface area light collection fraction of about 90%.

The DIRC occupies 80 mm of radial space in the central detector volume including supports and construction.
tolerances with a total of about 19% radiation length thickness at normal incidence. The radiator bars cover a solid angle corresponding to about 94% of the azimuth and 83% of the c.m. polar angle cosine.

3 DIRC Performance

The performance of the DIRC is influenced by two factors. First, information from the PMTs has to be separated into background and signal. Second, the $\theta_C$ resolution of the signal has to allow for the separation of different particle species.

Figure 3 shows a typical di-muon event ($e^+e^- \rightarrow \mu^+\mu^-$). In addition to the signals caused by Cherenkov light from the muon tracks, about 500 background signals can be seen in the 600 ns readout window centered around the trigger. This background is dominated by low energy photons from the PEP-II machine hitting the standoff box.

The time-to-digital converter (TDC) chip[12] used in the DIRC data readout is designed such that a dead time of about 5% occurs at an input rate of 250 kHz. Some care in machine tuning is required to stay under a limit of 250 kHz per tube. To monitor this rate, one PMT in each sector is read out via a scaler. Figure 4 shows the maximum scaler rate as a function of the PEP-II luminosity during data taking in 2000 and 2001. In March 2000 the accelerator operated at a peak luminosity of $10^{33}$ cm$^{-2}$ s$^{-1}$. Figure 4(a) shows, at a value corresponding to only one third of the design luminosity, the PMT rates reached a level that caused noticeable dead times. Due to those findings, lead shielding was installed in the summer of 2000 around the beam line components near the backward end-cap. Initially, localized shielding was added in the form of lead bricks which were stacked around the beam pipe and in front of a large quadrupole. This shielding significantly improved the background situation so that noticeable TDC dead times were reached only at $2.5 \times 10^{33}$ cm$^{-2}$ s$^{-1}$ (Figure 4(b)). During
the shutdown in January 2001, the localized lead brick shielding was replaced by an engineered, homogeneous lead shielding of 5 cm to 8 cm thickness covering the inside radius of the standoff box and is easily removable to facilitate access to the central detector and beam line components. As is shown in figure 4(c), the maximum scaler rates at luminosities of $4.2 \times 10^{33} \text{ cm}^{-2} \text{ s}^{-1}$ are well below the level that would cause TDC inefficiencies.

During the shutdown following the 2001-2002 run, we plan to replace the TDCs with a faster version with deeper buffering that is designed to have a deadtime of less than 5% at 2.5 MHz input rate, suitable for luminosities of at least $10^{34} \text{ cm}^{-2} \text{ s}^{-1}$.

The Dirc is intrinsically a three-dimensional imaging device. Photons are focused onto the phototube detection surface via a “pinhole” defined by the exit aperture of the bar, so that the photon propagation angles $\alpha_x$ and $\alpha_y$ can be measured in two-dimensional space, where $x$ (bar width) and $y$ (bar thickness) are the directions transverse to the bar axis. The travel time of the photon down the bar is also related to the photon propagation angle ($\alpha_z$) with respect to the bar axis. Imaging in the Dirc occurs in all three of these dimensions, by recording the time of the PMT signal. As the track position and angles are known from the tracking system, these three $\alpha$ angles can be used to determine the two angles ($\theta_C, \phi_C$). This over-constraint on the angles is particularly useful in dealing with ambiguities and high background rates.

The single photon resolution can be calculated from the geometrical, the chromatic and the transport term. The geometrical uncertainty is, for the pinhole optics of the Dirc, given by the standoff box size, the bar and the PMT size. With 7.2 mrad, it is the single biggest contribution to the single photon resolution. The chromatic uncertainty originates from the fact that the photons are produced with different wavelengths and, therefore, have different cone opening angles $\theta_C$. Using the range in photon wavelength accepted by the PMTs, the chromatic effect contributes to the resolution with 5.4 mrad. The final uncertainty comes from imperfections of the bars and the glue joints. This transport term is approximately 2 mrad to 3 mrad.

Combining the three contributions, a single photon resolution of $\sigma_{\theta_C, \gamma} = 9.5$ mrad is expected for the Dirc.
Figure 5: The difference between the measured and expected Cherenkov angle for single photons, $\Delta \theta_{C,\gamma}$, for single muons in $\mu^+\mu^-$ events. The curve shows the result of a fit of two Gaussians to the data. The width of the narrow Gaussian is 9.6 mrad.

Figure 5 shows the single photon angular resolution obtained from di-muon events. There is a broad background of less than 10% relative height under the peak that originates mostly from track-associated sources, such as $\delta$ rays, reflections off the glue-fused silica boundaries, and combinatorial background[13]. The width of the peak translates to a resolution of about 9.6 mrad, in good agreement with the expected value.

The resolution on the track Cherenkov angle is defined by a correlated term and the single photon resolution which scales with the number of photoelectrons:

$$\sigma_{\theta_C} = \sigma_{\theta_{C,\text{corr}}} + \frac{\sigma_{\theta_{c,\gamma}}}{\sqrt{N_{\text{pe}}}}$$  \hspace{1cm} (1)

where $N_{\text{pe}}$ is the number of photons detected per track.

The number of photoelectrons varies between 16 for small values of $\cos \theta_{\text{track}}$ at the center of the barrel and 60 at large values of $\cos \theta_{\text{track}}$ as is shown in Figure 6. This variation is well reproduced by Monte Carlo simulation and can be understood from the geometry of the DIRC. The number of Cherenkov photons varies with the path length of the track in the radiator, it is smallest at perpendicular incidence at the center and increases towards the ends of the bars. In addition, the fraction of photons trapped by total internal reflection rises with larger values of $\cos \theta_{\text{track}}$. This increase in the number of photons for forward going tracks is a good match to the increase in performance required at larger momentum.

With the present alignment, the track Cherenkov angle resolution for di-muon events is shown in Figure 7. The width of the fitted Gaussian distribution is 2.4 mrad compared to the design goal of 2.2 mrad.

The measured time resolution is 1.7 ns, close to the intrinsic 1.5 ns transit time spread of the PMTs. This resolution is used to efficiently distinguish background from signal photons but is not sufficient to improve the Cherenkov angle resolution.

Figure 8 shows an example of the use of the DIRC for particle identification. The $K\pi$ invariant mass spectra are shown with and without the use of the DIRC for kaon identification. The peak corresponds to the decay of the $D^0$ particle.

The PID performance of the DIRC has been studied with a sample of pions and kaons, selected kinematically using $D^0 \rightarrow K^-\pi^+$ decays from inclusive $D^*$ production.
Figure 6: Number of detected photons versus track polar angle for reconstructed tracks in di-muon events compared to Monte Carlo simulation. The mean number of photons in the simulation has been tuned to match the data.

Figure 7: Resolution of the reconstructed Cherenkov polar angle per track for di-muon events. The curve shows the result of a Gaussian fit with a resolution of 2.4 mrad.
The $\pi/K$ separation power of the DIRC was defined as the difference of the expected Cherenkov angles for pions and kaons, divided by the measured track Cherenkov angle resolution. As shown in Figure 9, the separation between kaons and pions at 3 GeV/c is about 4.4$\sigma$, within 10% of the design goal.

The efficiency for correctly identifying a charged kaon that traverses a radiator bar and the probability to wrongly identify a pion as a kaon are also determined from the inclusive $D^*$ sample and are shown as a function of the track momentum in Figure 10 for a particular choice of particle selection criteria. The kaon selection efficiency and pion misidentification, integrated over the $K$ and $\pi$ momentum spectra of the $D^*$ control sample, are $97.97 \pm 0.07\%$ (stat. only) and $1.83 \pm 0.06\%$ (stat. only), respectively.

A report on the operational experience with the DIRC detector can be found in [14].

4 **DIRC in Higher Luminosity Environment**

In a higher luminosity environment, the accelerator-induced background will cause the main challenge. From a set of special runs taken in February 2002, the background rate as a function of the beam currents $I_{\text{HER}}$ and $I_{\text{LER}}$ in the high and low energy ring, respectively, and the luminosity $\mathcal{L}$ can be parameterized as

$$R = 13 \frac{\text{kHz}}{A} I_{\text{HER}} + 18 \frac{\text{kHz}}{A} I_{\text{LER}} + 10 \frac{\text{kHz}}{10^{33} \text{ cm}^{-2} \text{ s}^{-1} \mathcal{L}}.$$

For the conditions at the beginning of this year, the current terms dominate but for higher luminosities, the corresponding term will contribute significantly. The anticipated limit of the luminosity PEP-II will be able to provide without major upgrade is $4 \times 10^{34} \text{ cm}^{-2} \text{ s}^{-1}$. With some upgrades to the shielding and the TDC upgrade,
Figure 9: DIRC $\pi/K$ separation versus track momentum measured in $D^0 \rightarrow K^-\pi^+$ decays selected kinematically from inclusive $D^*$ production.

Figure 10: Efficiency and misidentification probability for the selection of charged kaons as a function of track momentum, for a particular choice of particle selection criteria. The data use $D^0 \rightarrow K^-\pi^+$ decays selected kinematically from inclusive $D^*$ production.
the DIRC will be able to reliably work in this environment. At higher luminosities, such as expected after major PEP-II updates or for SuperBaBar, more changes will be necessary.

A solution to high background rates is to reduce the size of the standoff box. However, without modifications to the design, this would lead to an increase in the geometric resolution term and would cause a considerable decrease in the DIRC performance.

A modified design, as shown in figure 11, employs smaller sized photodetectors as well as focusing optics effectively removing the bar size uncertainty in the focusing plane. These two enhancements can be balanced so that the size of the standoff region can be reduced while keeping a similar or improved geometrical resolution.

In addition, smaller photodetectors with a better transit time spread will improve the timing resolution of the detector. This can be used to further reduce the background by using tighter time cuts and to reduce the chromatic uncertainty. The travel time of a photon is the difference between the time the particle hits the bar and the arrival time of the photon. It depends on the path length and the group velocity in the transit medium. The group velocity itself depends on the refractive index. Thus, the travel time and path length yield a measure of the wavelength of the photon. Figure 12 shows a calculation demonstrating that a timing resolution in the order of 100 ps is needed for a significant improvement in the chromatic uncertainty.

Reducing the range of wavelength accepted in the detection system will reduce the range of Cherenkov cone opening angles contributing and, thus, reduce the chromatic uncertainty. The drawback of this solution is the loss in the number of photons detected per track causing a reduced suppression of the single photon resolution term. These two effects can be balanced in order to reach the optimal total $\theta_C$ resolution.

With a timing resolution in the order of 100 ps, the ratio of the track to detector distance over the path length will provide an additional measure of the photon angle. In some regions of phase space, especially at small dip angles, its resolution will be competitive to the angle resolution from the position of the PMT hit.

A more detailed discussion can be found in [15].

One of the photon detector candidates is the flat panel PMT H-8500 by Hamamatsu[16]. It has $8 \times 8$ square pads on a size of $50 \text{ mm} \times 50 \text{ mm}$. This leads to a high area efficiency and packaging density. The timing resolution is expected to be in the range of 100 ps to 200 ps. The disadvantage of the currently available model
Figure 12: Achievable wavelength resolution as a function of photon wavelength assuming 100 ps and 500 ps timing resolution.

is its low gain in the order of $1.6 \times 10^6$.

Studies of the timing resolution on an early pre-production version were encouraging. The time was measured at two thresholds for each signal in order to perform a time walk correction. The corrected time distribution[17] is shown in figure 13. A fit to a double Gaussian plus a second order polynomial describes the data well. The narrow Gaussian has a width of 125 ps. This value is not yet corrected for the light pulse width and instrumental effects. In addition, the double threshold method limits the data to PMT signals with a pulse height above the higher threshold. This removes some fraction of low signal events.

Currently, studies of the efficiency uniformity of the PMT area are in process and results will be available in near future.

5 Improvements for Future DIRC Detectors

The design described in the previous section will be sufficient to provide the required resolution of the DIRC for possible upgrade scenarios. However, for the SuperB environment with a design luminosity of $10^{36} \text{cm}^{-2} \text{s}^{-1}$, the projected occupancy in the tracking system makes building a completely new detector necessary.

This allows to reconsider the radiator and light guide design. Synthetic fused silica is still the material of choice as it fulfills all requirements in terms of transparency, radiation hardness, achievable uniformity in material and optical finish. In addition, it has a small radiation length which is benificial for a calorimeter outside of the DIRC system.

Increasing the thickness of the radiators will lead to an increased number of photons per track but it will also increase the amount of material in front of the calorimeter, so the thickness of the radiator can not be changed significantly.

Increasing the width of the radiators, such as using one plate instead of several bars, has advantages in the geometrical term of the single photon resolution. In a plate geometry, there are less side bounces and the path length for a photon measured in a given PMT with a known track position changes drastically with each
additional side bounce. Therefore, the hit time can be used to determine the number of side bounces and because of this the exit position of the photon at the instrumented bar end can be inferred. This is shown in figure 14, where the full line and the dashed line have significantly different path lengths.

There are a few examples in the following on the expected resolution for the different setups. A detailed discussion of the geometries can be found in [15]. Please note that the resolutions are given in terms of the photon exit angles $\alpha$ at the end of the bar or plate. These are different to the Cherenkov angle resolution $\theta_C$. However, there is a strong correlation between $\sigma_{\alpha_y}$ and $\sigma_{\theta_C}$ while the correlation between $\sigma_{\alpha_x}$ and $\sigma_{\theta_C}$ is weaker.

**Current BaBar DIRC**

The current DIRC setup has round PMTs with 29 mm diameter and rectangular bars of size 35 mm × 17.5 mm.
The resolution on the photon exit angle at the edge of the bar is

$$\sigma_{\alpha_x} \approx \frac{1}{L_{SOB}} \sqrt{\sigma_x^2(\text{bar}) + \sigma_x^2(\text{pixel})} \approx \frac{1}{1170 \, \text{mm}} \sqrt{\frac{1}{12}(35 \, \text{mm})^2 + \frac{1}{16}(29 \, \text{mm})^2} = 10.6 \, \text{mrad} \quad (3)$$

and

$$\sigma_{\alpha_y} \approx 7.6 \, \text{mrad} \quad (4)$$

The interface fused silica — water magnifies the angles thus improving the resolution by approximately 10% leading to $\sigma_{\alpha_{x/y}} = 9.5 \, \text{mrad}/6.9 \, \text{mrad}$.

**Focusing optics for BaBar like DIRC**

A focusing optic in $y$ with a pixel size of $6 \, \text{mm} \times 6 \, \text{mm}$ and a corresponding standoff distance of $L = 250 \, \text{mm}$ leads to

$$\sigma_{\alpha_y} \approx \frac{1}{L} \sqrt{\sigma_y^2(\text{pixel})} \approx \frac{1}{250 \, \text{mm}} \sqrt{\frac{1}{12}(6 \, \text{mm})^2} = 6.9 \, \text{mrad} \quad (5)$$

similar to the current $\alpha_y$ resolution. The resolution in $x$ will get worse as focusing in both dimensions would complicate ambiguity resolution. This can be compensated by the reduced chromatic uncertainty.

**Focusing optics with plates for SuperBaBar**

In order to improve the resolution, a smaller pad size of $2 \, \text{mm}$ in $y$ direction and $6 \, \text{mm}$ in $x$ direction can be used. The resolution can be described by

$$\sigma_{\alpha_y} \approx \frac{1}{L} \sqrt{\sigma_y^2(\text{pixel})} \approx \frac{1}{250 \, \text{mm}} \sqrt{\frac{1}{12}(2 \, \text{mm})^2} = 2.3 \, \text{mrad} \quad (6)$$

in $y$ direction and in $x$

$$\sigma_{\alpha_x} \approx \frac{1}{L} \sqrt{\sigma_x^2(\text{track}) + \sigma_x^2(\text{pixel})} \approx \frac{1}{1000 \, \text{mm}} \sqrt{\frac{(4 \, \text{mm})^2 + \frac{1}{12}(6 \, \text{mm})^2} = 4.3 \, \text{mrad} \quad (7)$$

In the last equation $L$ is the length of the region where the photon can expand without side bounces. This length varies depending on the number and positions of the side bounces.

Together with the improved chromatic resolution, this leads to a significant improvement in the single photon resolution compared to the current BaBar DIRC.

The major uncertainty not directly related to the DIRC design is the correlated uncertainty on the position of the track at the entry into the radiator. In order to improve the particle separation, it is not sufficient to improve the intrinsic DIRC uncertainty only. A possible solution is to add a tracking device outside the DIRC volume. This would also allow for finding particle conversions and decays inside the radiator material.

A further improvement is to enlarge the angular coverage of the particle identification system by using an end-cap device. The DIRC covers the barrel region only. Additional challenges for an end-cap device are the limited amount of space in the end-cap, the higher radiation levels close to the beam-pipe, and that the readout has to be done inside the magnetic field which makes standard PMTs unusable. Interesting alternative photodetectors have been suggested but they still need to be studied in detail before an evaluation on the feasibility of an end-cap DIRC can be performed.
6 Conclusions

The DIRC is a novel particle identification system used for the first time in the Babar environment. It is performing close to the design and has a significant influence on most physics analysis.

Increasing the luminosity beyond the Babar design values will result in challenges for the DIRC system mainly due to increased background levels of low energy photons from PEP-II. Improvements in shielding and in the maximal data taking rate will allow for running the current detector up to the anticipated PEP-II limits. Beyond that, reducing the size of the standoff box will be necessary. In order to keep the Cherenkov angle resolution on the design level, the standoff box needs to be replaced by focusing optics with smaller sized photodetectors. Timing resolution in the order of 100 ps is vital to reduce the chromatic uncertainty and can effectively separate signal from background photons. Research on candidate devices has started and first tests have shown promising results.

At luminosities in the order of $10^{36} \text{cm}^{-2} \text{s}^{-1}$ as envisioned for SuperBabar, a completely new DIRC can be built. Fused silica plates instead of bars and even smaller PMT pad sizes along with an improved tracking will allow for significant improvements in the Cherenkov angle resolution.

Enlarging the angular coverage of a DIRC particle identification system will require an end-cap device. The challenges for this device include photodetection inside of the magnetic field and the limited amount of space prohibiting large expansion volumes.

References


1Stanford Linear Accelerator Center, Stanford, CA 94309, USA.
2CEA, DAPNIA, CE-Saclay, F-91191, Gif-sur-Yvette Cedex, France.
3LPNHE des Universités Paris 6 et Paris 7, Tour 33, Bc 200, 4 Place Jussieu, F-75252, Paris, Cedex 05, France.
4LAL Orsay, Université Paris Sud, Batiment 200, F-91405 Orsay Cedex, France.
5LPNHE de l’Ecole Polytechnique, Route de Saclay, F-91128 Palaiseau Cedex, France.
6Lawrence Berkeley National Laboratory, One Cyclotron Road, Berkeley, CA 94720, USA.
7Dept. of Physics, University of California, Santa Barbara, CA 93106, USA.
8Dept. of Physics, Colorado State University, Fort Collins, CO 80523, USA.
9Dept. of Physics, University of Cincinnati, Cincinnati, OH 45221, USA.

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[5] Spectrosil is a trademark of TSL Group PCL, Wallsend, Tyne on Wear, NE28 6DG, England; Sold in the USA by Quartz Products Co., Louisville, KY, USA.

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